

Efficiency analysis of a capacitor charging power supply for a pulsed klystron-modulator*

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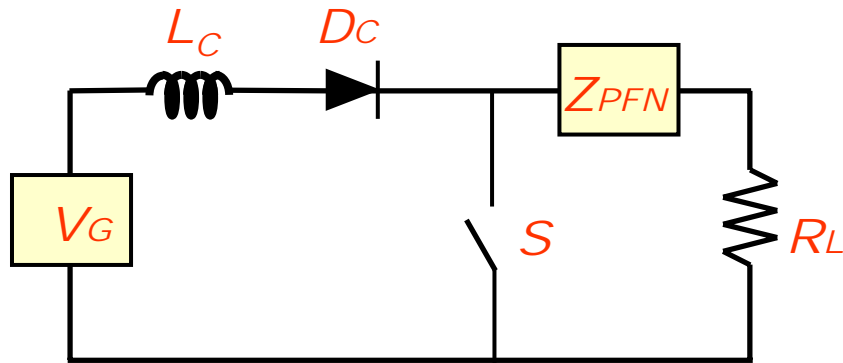
Abstract

A current source, inverter power supply is best choice for a capacitor-charging power supply of a pulsed klystron-modulator. Its high frequency technology makes the system size small and the regulation fine. The command-charging feature of the inverter guarantees higher reliability of switching function.

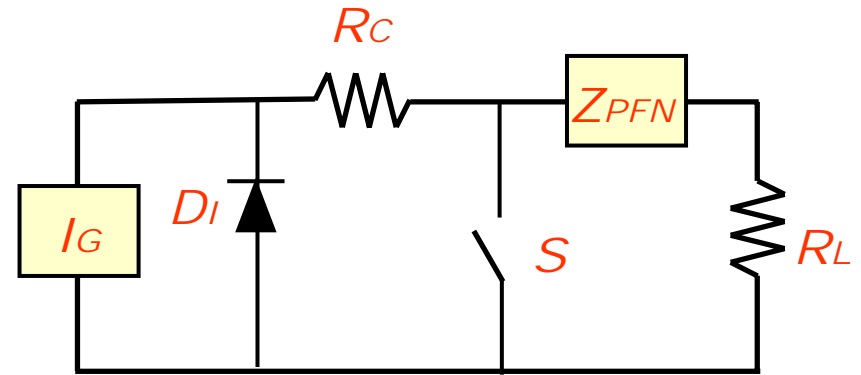
Thermal design is most critical in this power supply so the analysis of the system efficiency is essential. Better efficiency can be obtained through accurate evaluation of power loss distribution.

Design and fabrication detail of an air-cooled 50-kV, 15-kW inverter charging supply are presented. The efficiency and the stability of the power supply are estimated and examined.

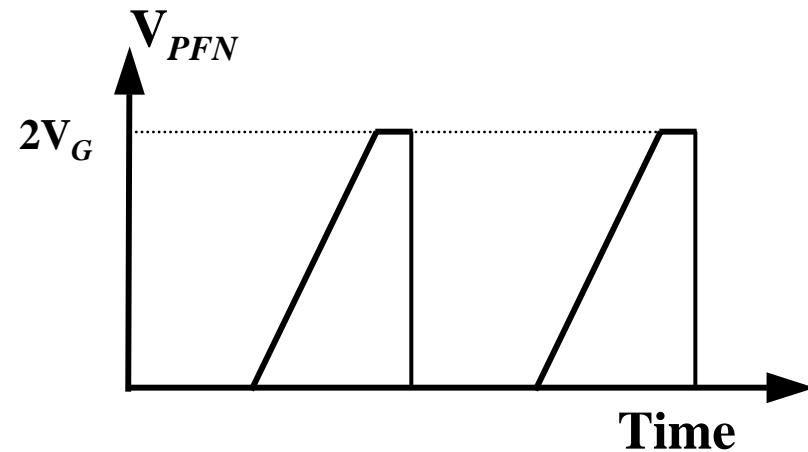
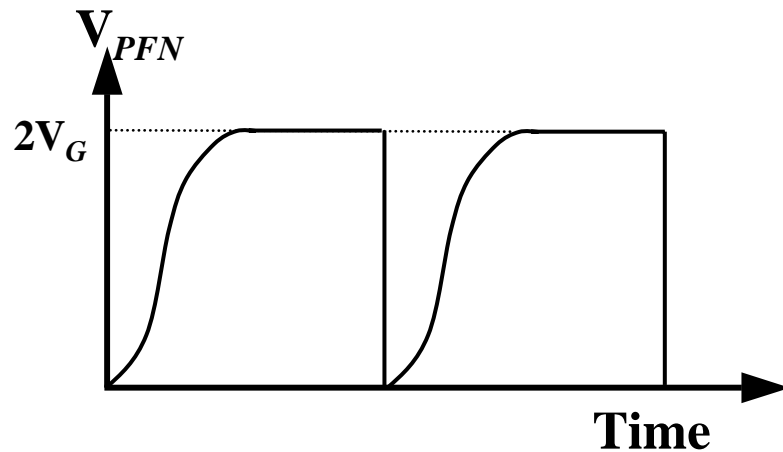
Line-type Modulator & Charging Waveform



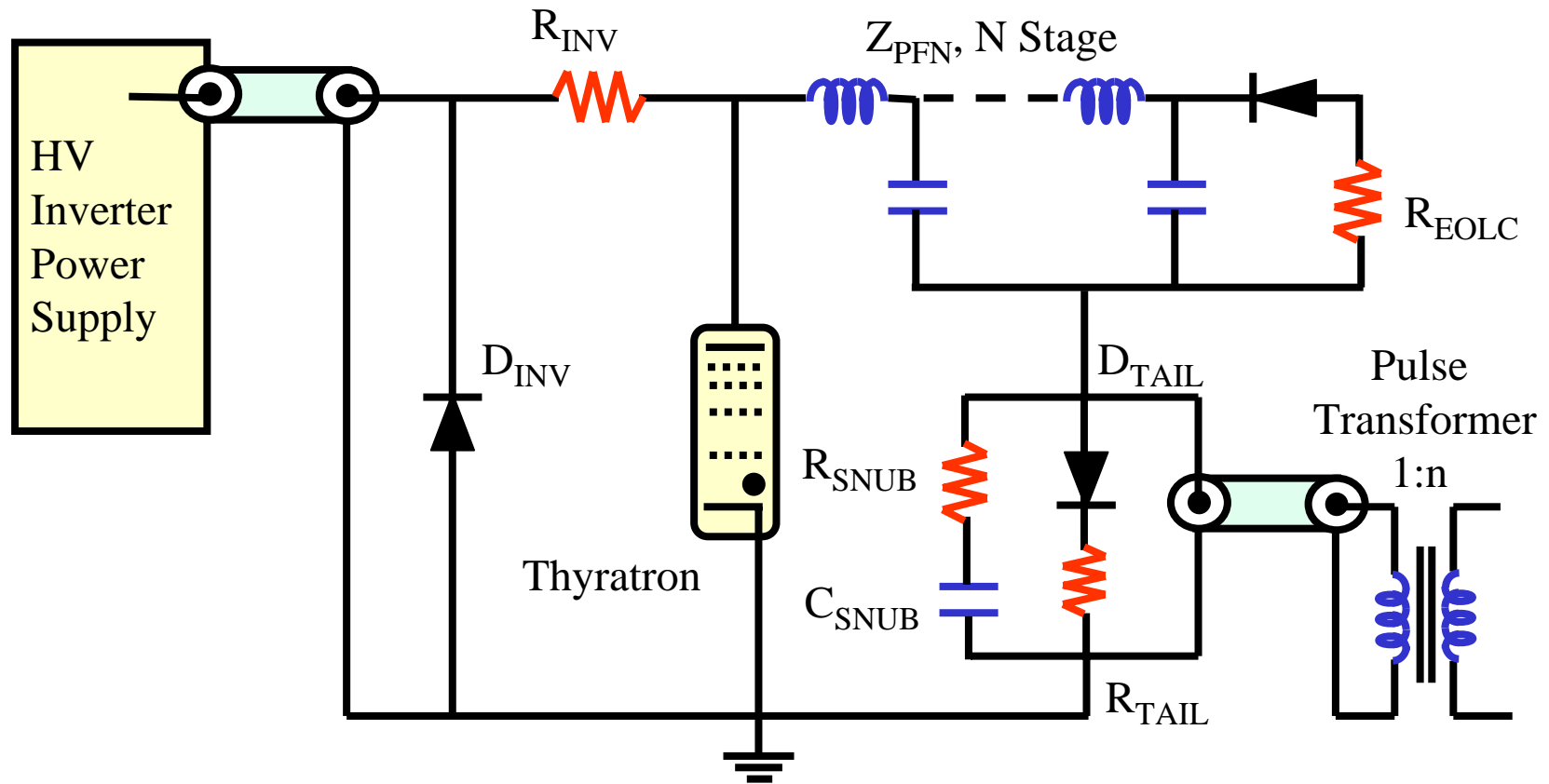
Voltage Source



Current Source



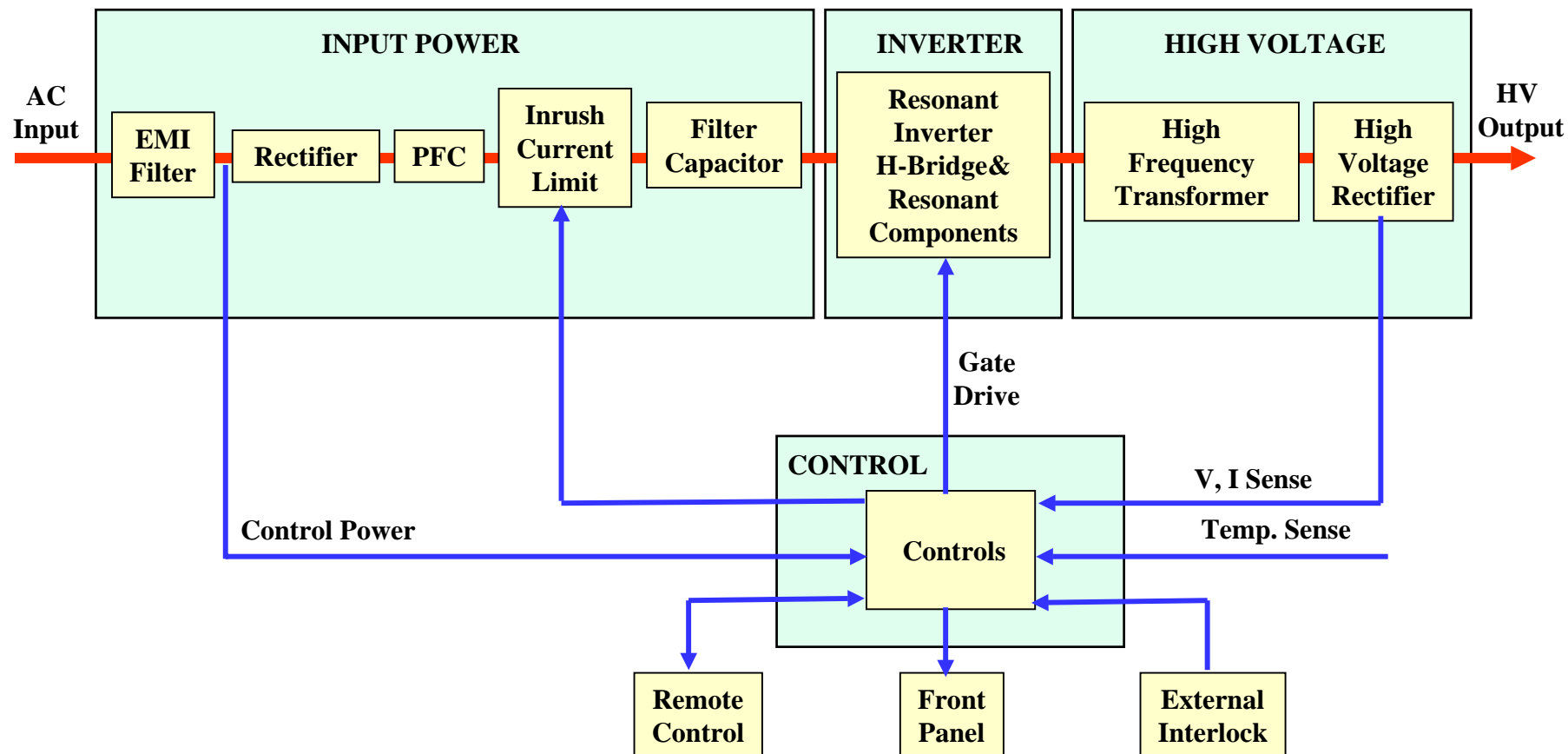
Modulator Layout with a Inverter Power Supply



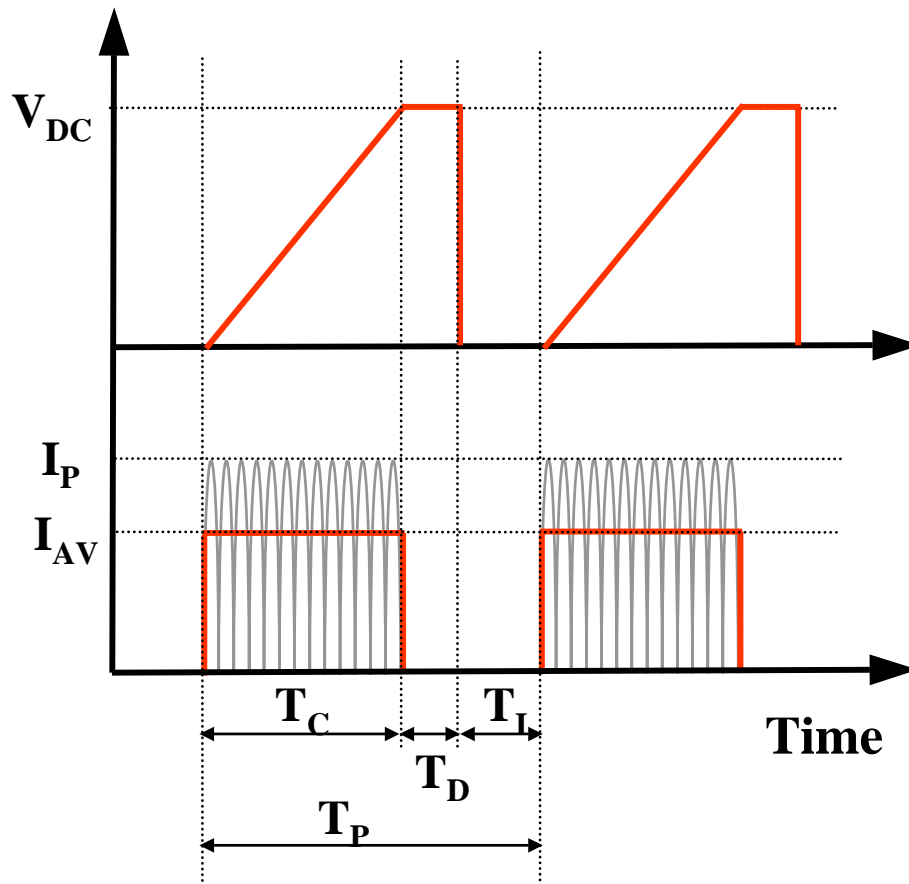
Key Features with a Inverter Power Supply

- **High Reliability by Command Charging Function**
- **Short Circuit Protection**
- **Small Size by High Frequency Utilization**
- **Expandability by Parallel Operation**
- **Easy Maintenance by a Dead Module Replacement**
- **Flexible Control Interface**
- **Removal of a Lossy De-Q'ing System**
- **Removal of a Bulky EOLC Thyrite**

Block Diagram of a Inverter Power Supply



Design Basics



Power Supply;

$$P_O = \frac{1}{2} V_{DC} I_{AV} = \frac{1}{\pi} \frac{V_{DC}^2}{Z} = f_r E_r$$

$$I_{AV} = \frac{2}{\pi} I_P, \quad I_P = \frac{V_{DC}}{Z}, \quad E_r = \frac{1}{2} C_r (2V_{DC})^2$$

Load;

$$P_O = E / T_C = \text{peak power [J/sec]}$$

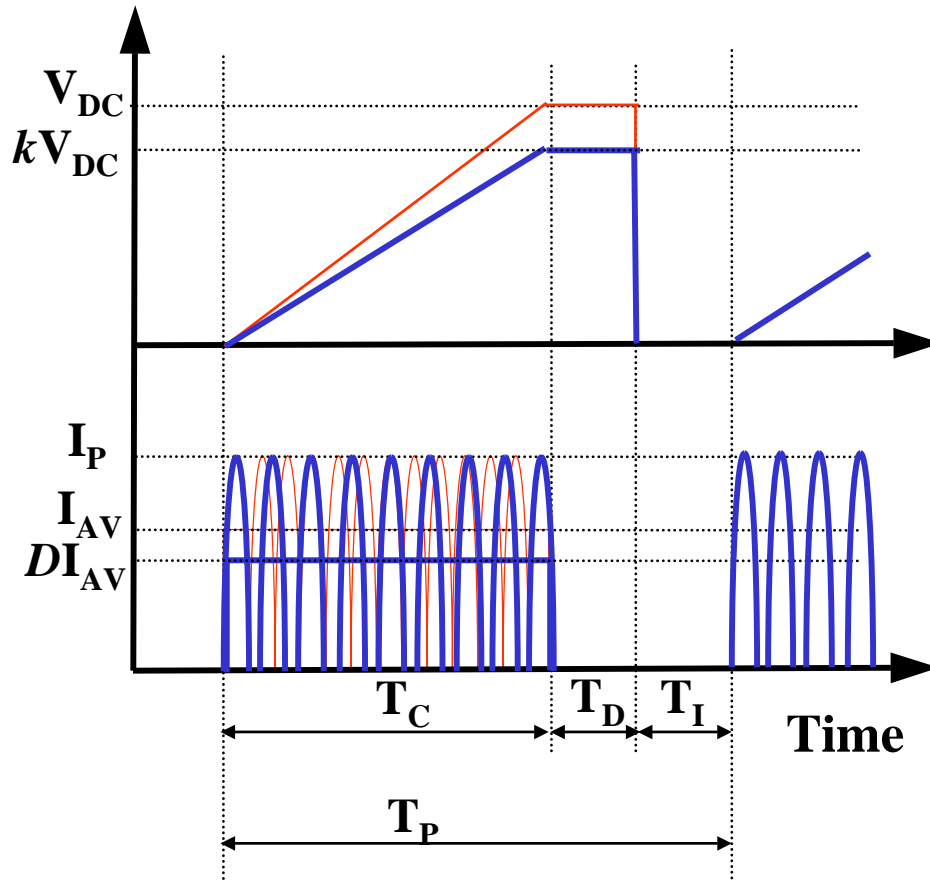
$$P_{av} = E / T_P = \text{average power [W]}$$

$$E = (1/2) C V_{DC}^2, \quad C = \text{load capacitance [F]}$$

$$T_P = \text{period, } T_C = \text{charging time}$$

$$T_D = \text{dwell time, } T_I = \text{dead time}$$

Voltage Utilization & Switching Duty



$$P_{AV} = P_{PEAK} D = \frac{1}{\pi} \frac{V_{DC}^2}{Z} k d D$$

$$P_{PEAK} = \frac{1}{2} (k V_{DC}) I_{AV} = \frac{1}{\pi} \frac{V_{DC}^2}{Z} k d = f_r E_r k d$$

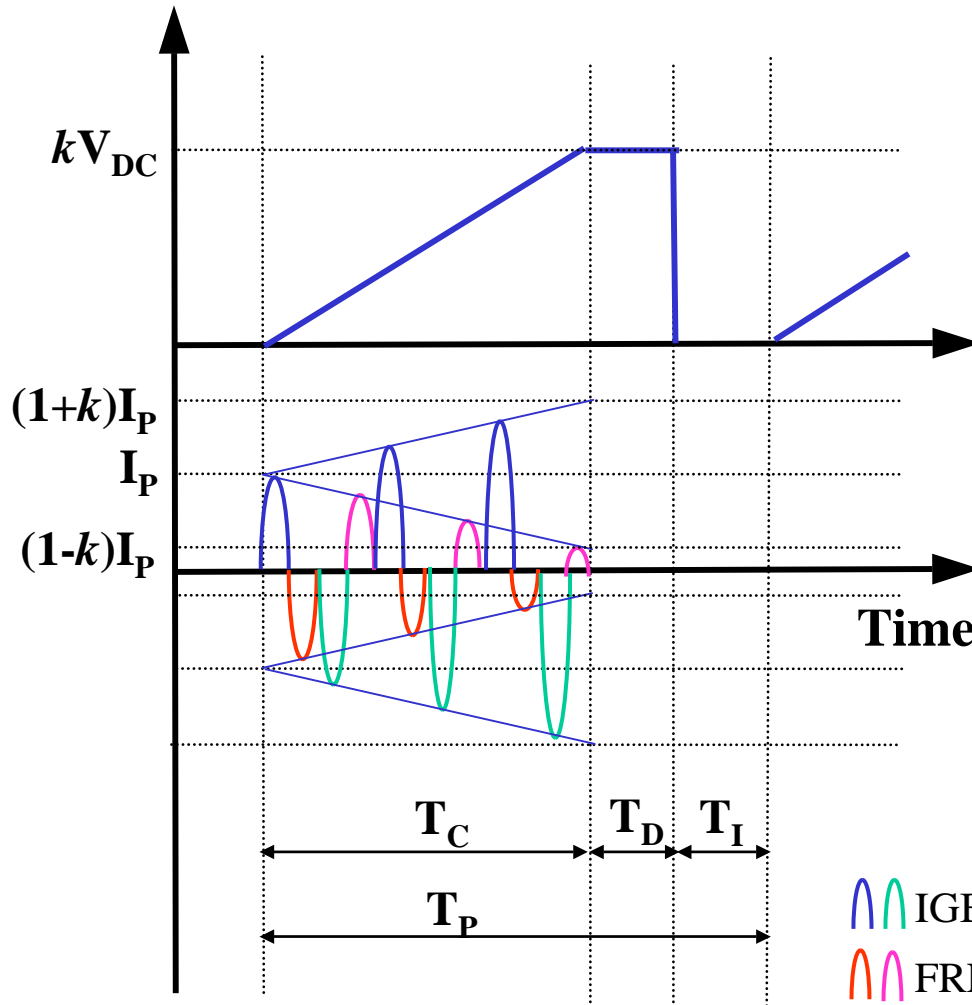
$$I_{AV} = \frac{2}{\pi} I_P d, \quad I_P = \frac{V_{DC}}{Z}, \quad E_r = \frac{1}{2} C_r (2V_{DC})^2$$

k ; Voltage utilization factor = V_o / V_{DC}

d ; Switching duty = f_{sw} / f_r

D ; Charging cycle duty = T_c / T_p

Resonant Current & Device Current



$$I_{AVG} = \frac{2}{\pi} I_P d D, \quad I_{RMS} = \frac{1}{\sqrt{2}} I_P \sqrt{d D}$$

$$I_{AVG,IGBT} = \frac{1}{2} \frac{2+k}{2} I_{AVG}$$

$$I_{AVG,FRED} = \frac{1}{2} \frac{2-k}{2} I_{AVG}$$

$$I_{RMS,IGBT} = \sqrt{1+k + \frac{k^2}{3}} \sqrt{\frac{1}{2}} I_{RMS}$$

$$I_{RMS,FRED} = \sqrt{1-k + \frac{k^2}{3}} \sqrt{\frac{1}{2}} I_{RMS}$$

$$I_{AVG,TOTAL} = I_{AVG}, \quad I_{RMS,TOTAL} = \sqrt{2\left(1 + \frac{k^2}{3}\right)} I_{RMS}$$

$$P_{IGBT} = 2V_{CE} I_{AVG,IGBT}, \quad P_{FRED} = 2V_f I_{AVG,FRED}$$

IGBT Current

FRED Current

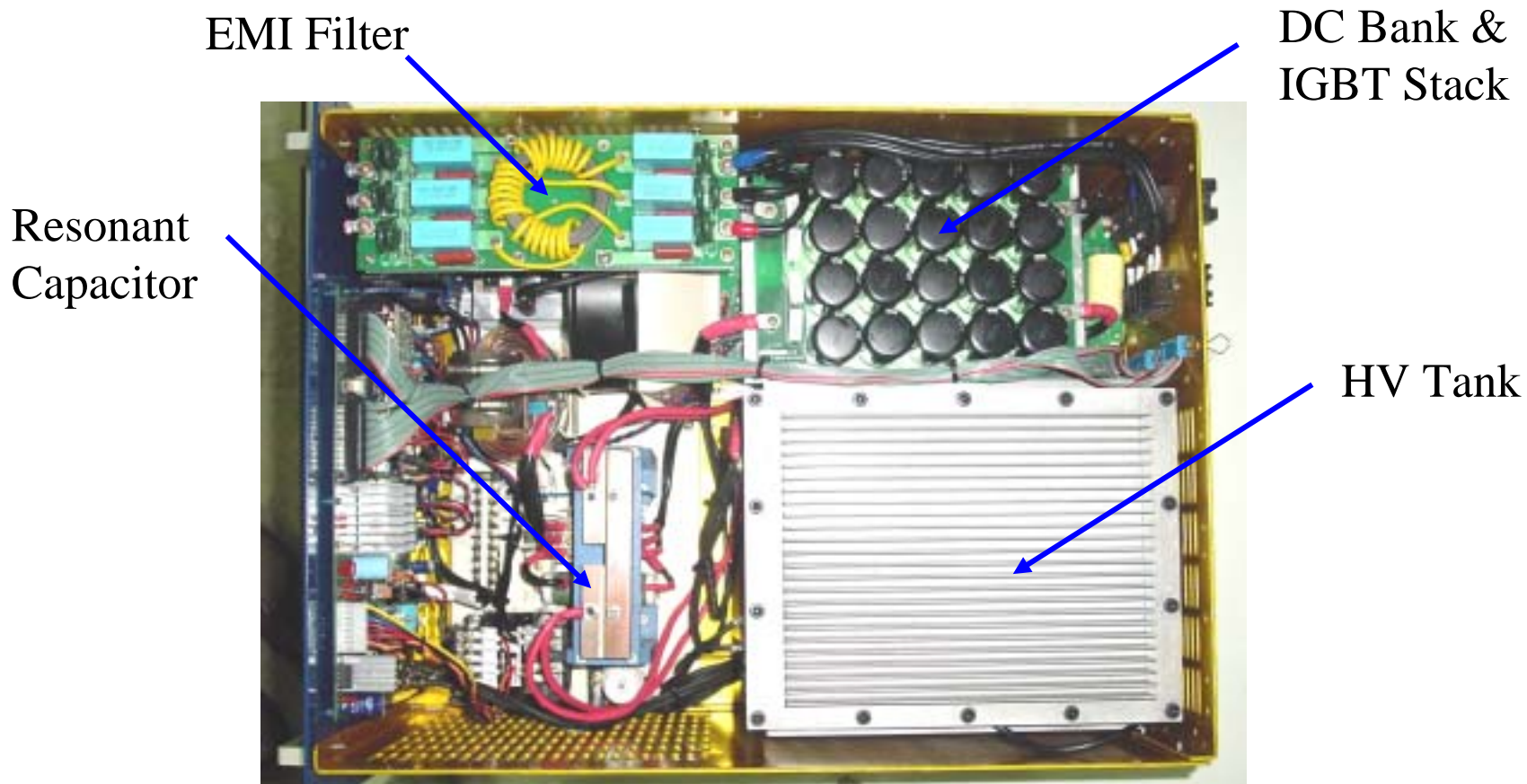
Capacitor-Charging Power Supply

SMART 5015

- Average Output Power [kW] 15
- Peak Charging Rate [kJ/s] 18
- Maximum Output Voltage [kV] 50
- Average Output Current [A] 0.6
- AC Input Voltage [V_{RMS}] 480
- Efficiency [%] 94
- Switching Frequency [kHz] 34.5
- Power Factor 0.85
- Air cooling
- 19" rack x 311 mm x 560mm
- 40 kg

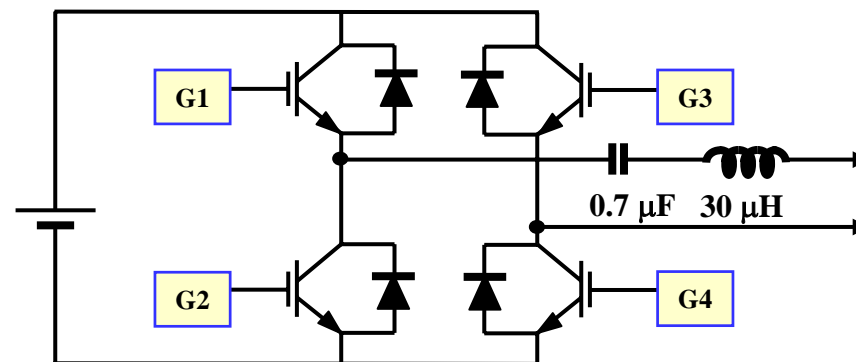


Photograph of Inverter Power Supply



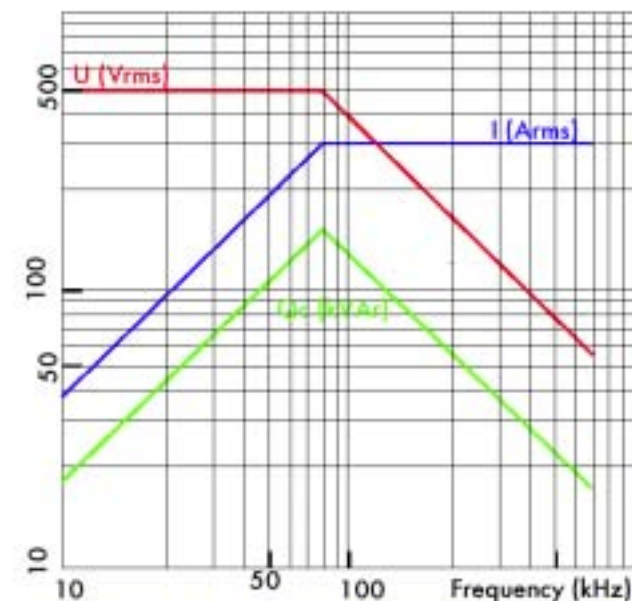
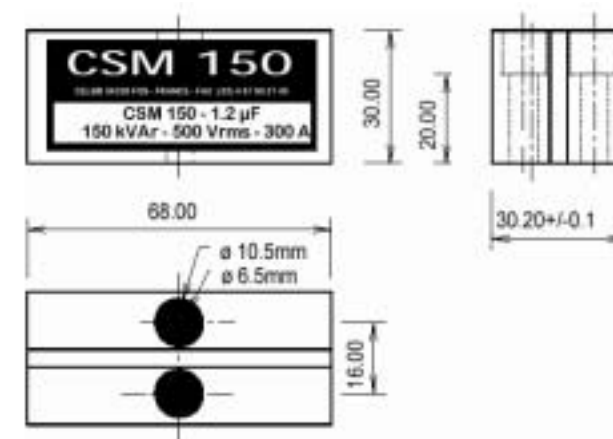
Inverter Specifications

Full Bridge, Series Resonant Converter



Resonant Frequency	35	[kHz]
Resonant Impedance	6.5	[Ω]
Resonant Capacitance	0.7	[μF]
Resonant Inductance	30	[μH]
Switch On-Time	14	[μs]
DC Bank Voltage	650	[V_{DC}]
Peak Switching Current	200	[A]
RMS Switching Current	74	[A]
Average Switching Current	52.5	[A]

Resonant Capacitor CSM 150

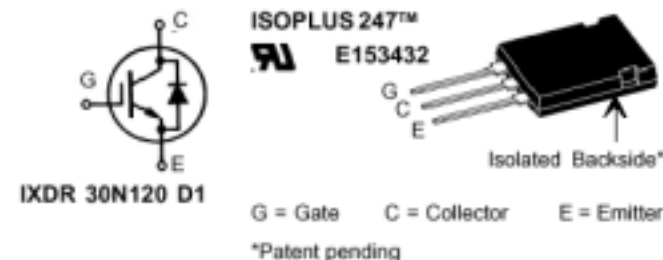


CSM/CSP 150 1.2 μ F - 500 Vrms - 300 Arms - 150 kVAr

Celem Power Capacitor Conduction Cooled Polypropylene

- Capacitance 1.2 [μ F]
- Maximum Voltage 500 [Vrms]
- Maximum Current 300 [Arms]
- Maximum Power 150 [kVAr]
- Frequency Limit 700 [kHz]
- Stray Inductance < 3 [nH]
- Weight 300 [g]
- Dimension [mm] 68 x 30 x 30.2

IGBT Switch



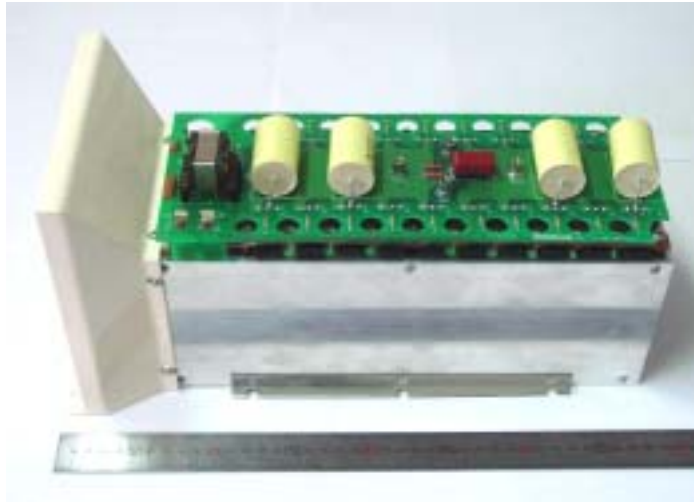
IGBT IXYS IXDR 30N120 D1

Vces, Collector-Emitter Voltage	1200	[V]
Ic, Continuous Collector Current @ Tc=90°C	30	[A]
Vce(ON), Collector-Emitter ON Voltage	2.4	[V]
Rjc, Junction to Case Thermal Impedance	0.6	[°C/W]
Tj, Maximum Junction Temperature	150	[°C]
Td(on), Gate Turn-On Delay	100	[ns]
Tr, Current Rise Time	70	[ns]
Td(off), Gate Turn-Off Delay	500	[ns]
Tf, Current Fall Time	70	[ns]

Diode

Vf, Maximum Forward Voltage	2.5	[V]
Qrr, Reverse Recovery Charge	2000	[nC]
Trr, Reverse Recovery Time	200	[ns]

IGBT Stack Cooling



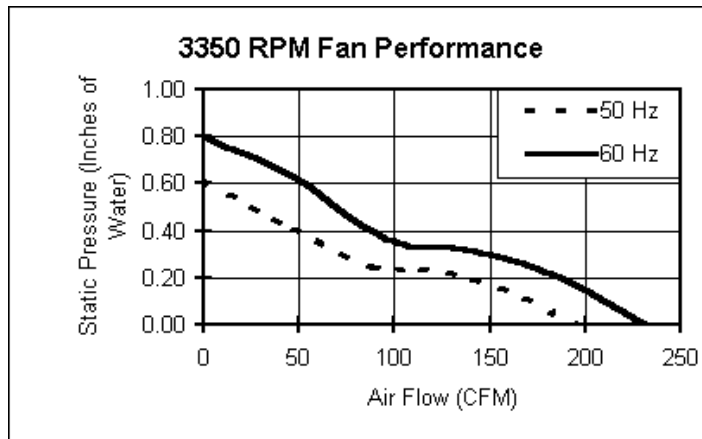
N; channel number S; channel space [in.]
 D; channel width [in.] H; channel length [in.]
 P; power [W], Q; air flow rate [CFM]
 DTa; air temperature rise [°C]
 DPa; pressure drop [in. H₂O]
 DTs; heat sink temperature rise [°C]

Forced convection

$$Q = 1.74 P / DTa$$

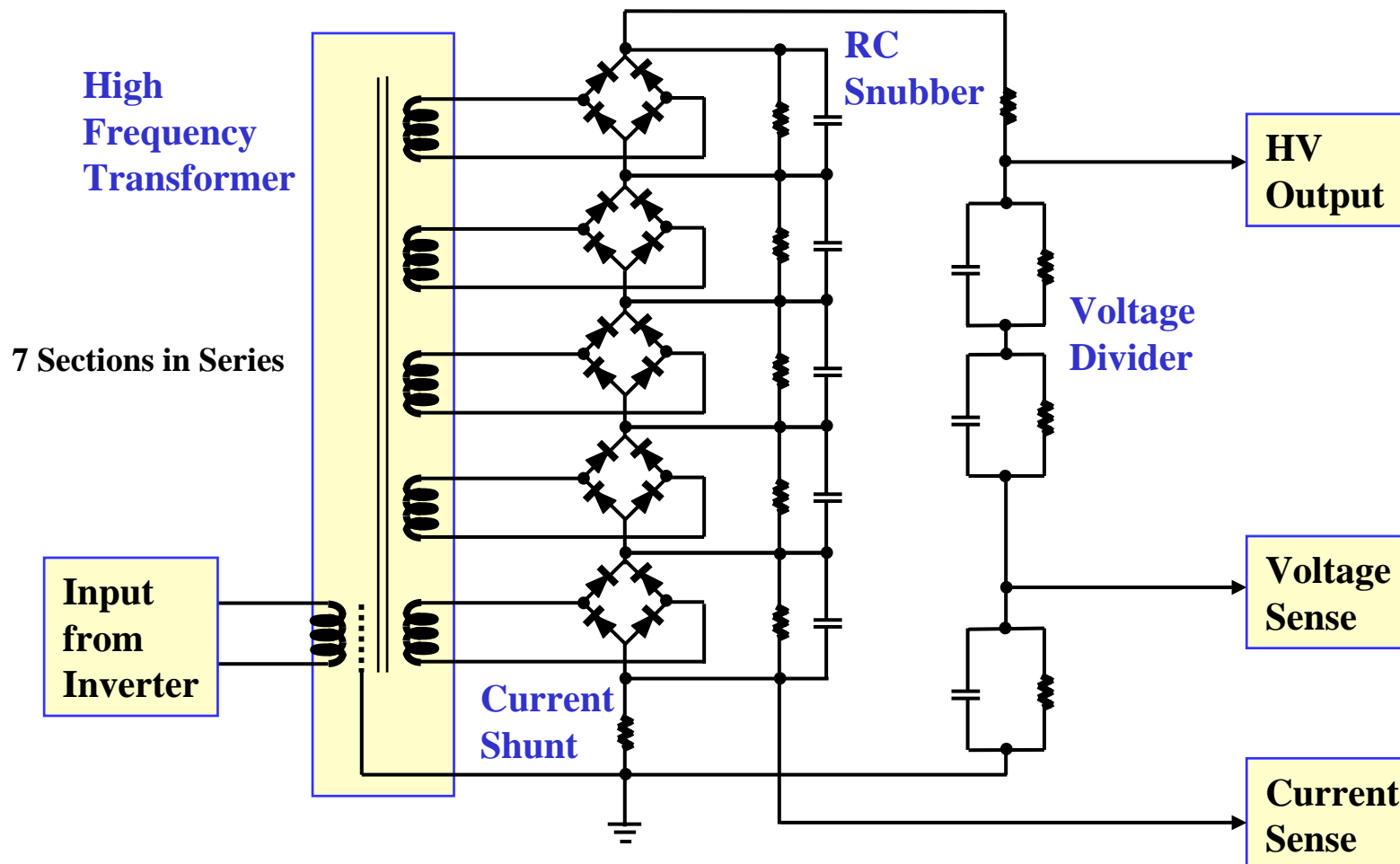
$$DPa = 0.001 Q^2 / (NSD)^2 \times [1 + 0.01 (H/S)]$$

$$DTs = 140 [S / (N^{0.2} D^{0.2} H)] \times (P / Q^{0.8})$$



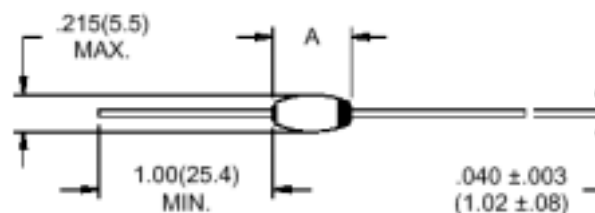
N (channel)		30.00
s (channel thickness)	in	0.16
d (channel width)	in	4.57
h (channel length)	in	11.81
DTa (air temp. diff)	degC	4.00
P (heat)	W	350.00
F (heat removal flow)	CFM	152.25
DP (air press. drop)	in H2O	0.09
DTs (heat sink temp. rise)	degC	4.38
Rth (forced air cooling)	degC/W	0.01

Schematic Diagram of High Voltage Section



HV Rectifier Diode

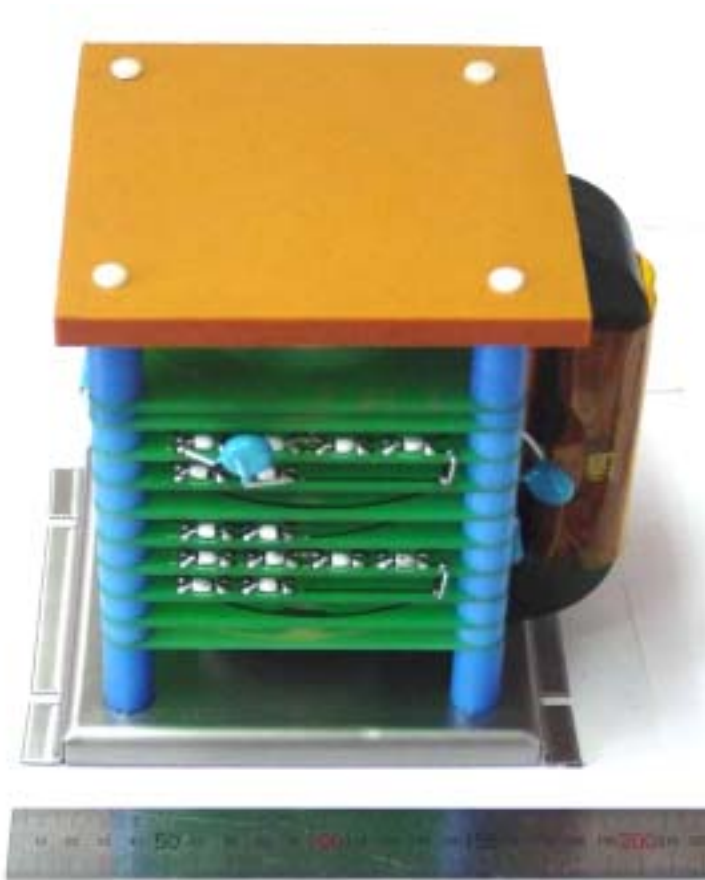
VMI Z50FG



Part	A
Z25FG Z50FG	.350(8.89) MAX.
Z100FG	.400(10.16) MAX.

V_r, Maximum DC Reverse Voltage	5000	[V]
I_o, Average Rectified Current @ T_L=55 °C	1.0	[A]
I_r, Reverse Leakage Current @ T_L=100°C	25	[uA]
I_{fsm}, 1 Cycle Surge Current @ T_L=25 °C, 8.3ms	8	[A]
V_f, Maximum Forward Voltage	9.0	[V]
T_j, Maximum Junction Temperature	150	[°C]
R_{jl}, Junction to lead Thermal Impedance	6 [°C/W] @ L = 3mm, 12 [°C/W] @ L = 6mm	
Q_{rr}, Reverse Recovery Charge	100	[nC]
T_{rr}, Reverse Recovery Time @ T_c=125°C	200	[ns]
I_{rrm}, Reverse Recovery Current	1	[A]
C_j, Junction Capacitance @ T_c=25 °C	16	[pF]

High Voltage Transformer & Rectifier



A. Construction

Core : TDK PE22 UU120x160x21 (2ea)

Primary : 24 turns, Litz wire

$L_p = 3.8$ [mH], $B = 3260$ [Gauss]

Secondary : 2100 turns, 7 section

Rectifier : VMI Z50FG

B. Leakage Inductance, L_l

$L_l = 4 \pi N_p^2 U_m (\Delta_{\text{gap}} + \Sigma \delta_i / 3) / L_m = 21 \mu\text{H}$

$N_p = \text{Primary Turns} = 24$

$U_m = \text{Mean Circumference of windings} = 20 \text{ cm}$

$\Delta_{\text{gap}} = \text{Gap Length between Windings} = 1 \text{ cm}$

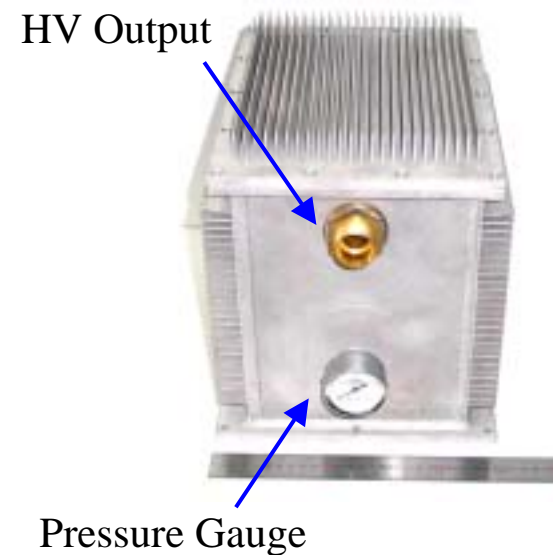
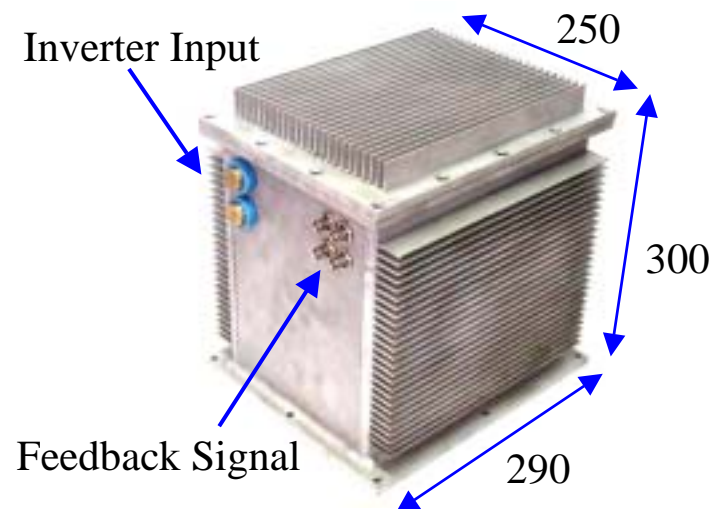
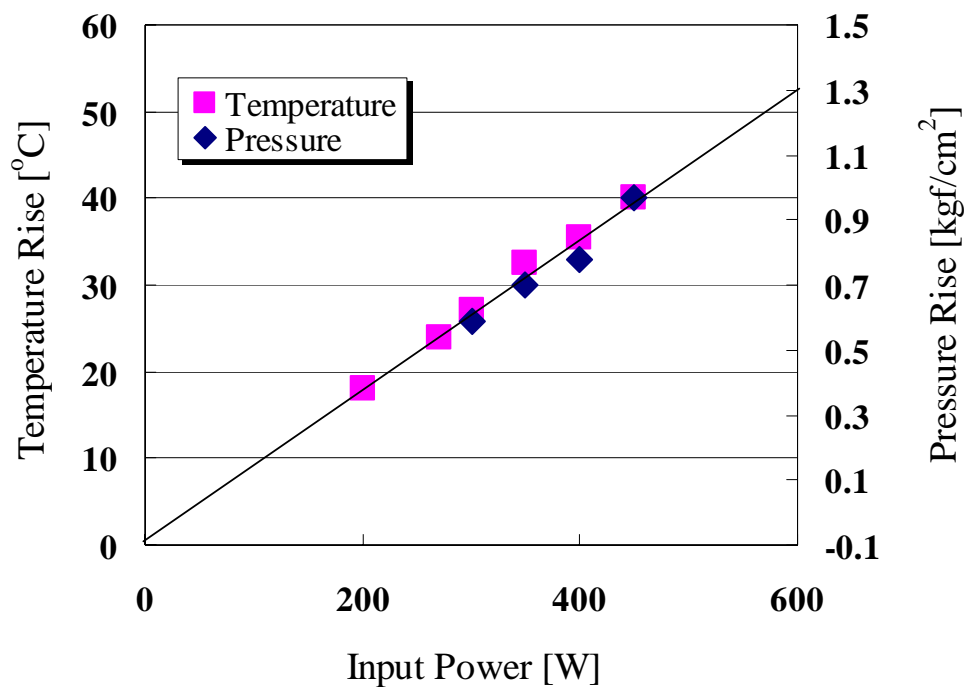
$\delta_i = \text{Thickness of Windings} = 1 \text{ cm}$

$L_m = \text{Winding Length} = 9 \text{ cm}$

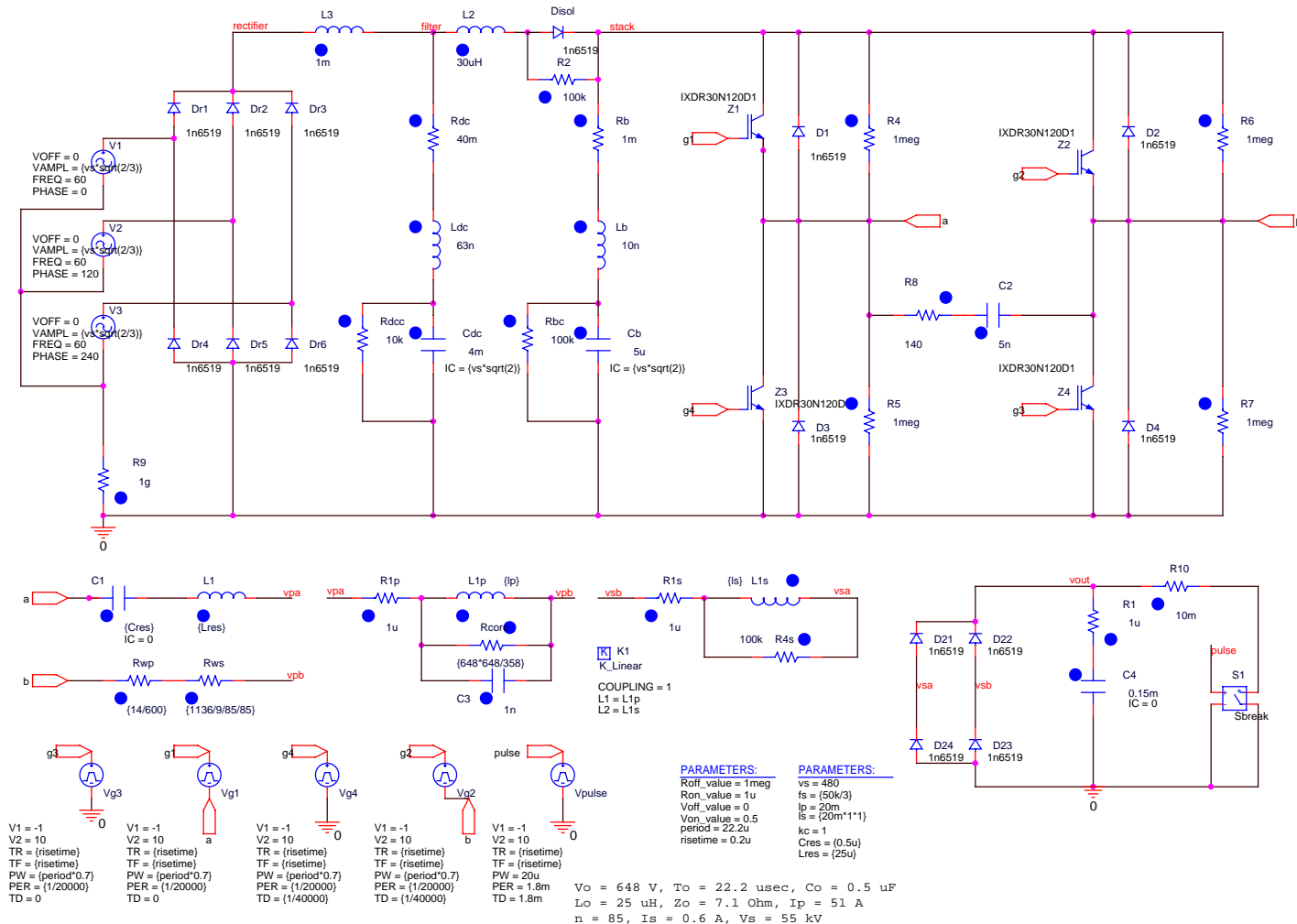
HV Tank Cooling

Internal Dimension; 25 x 21 x 21 cm

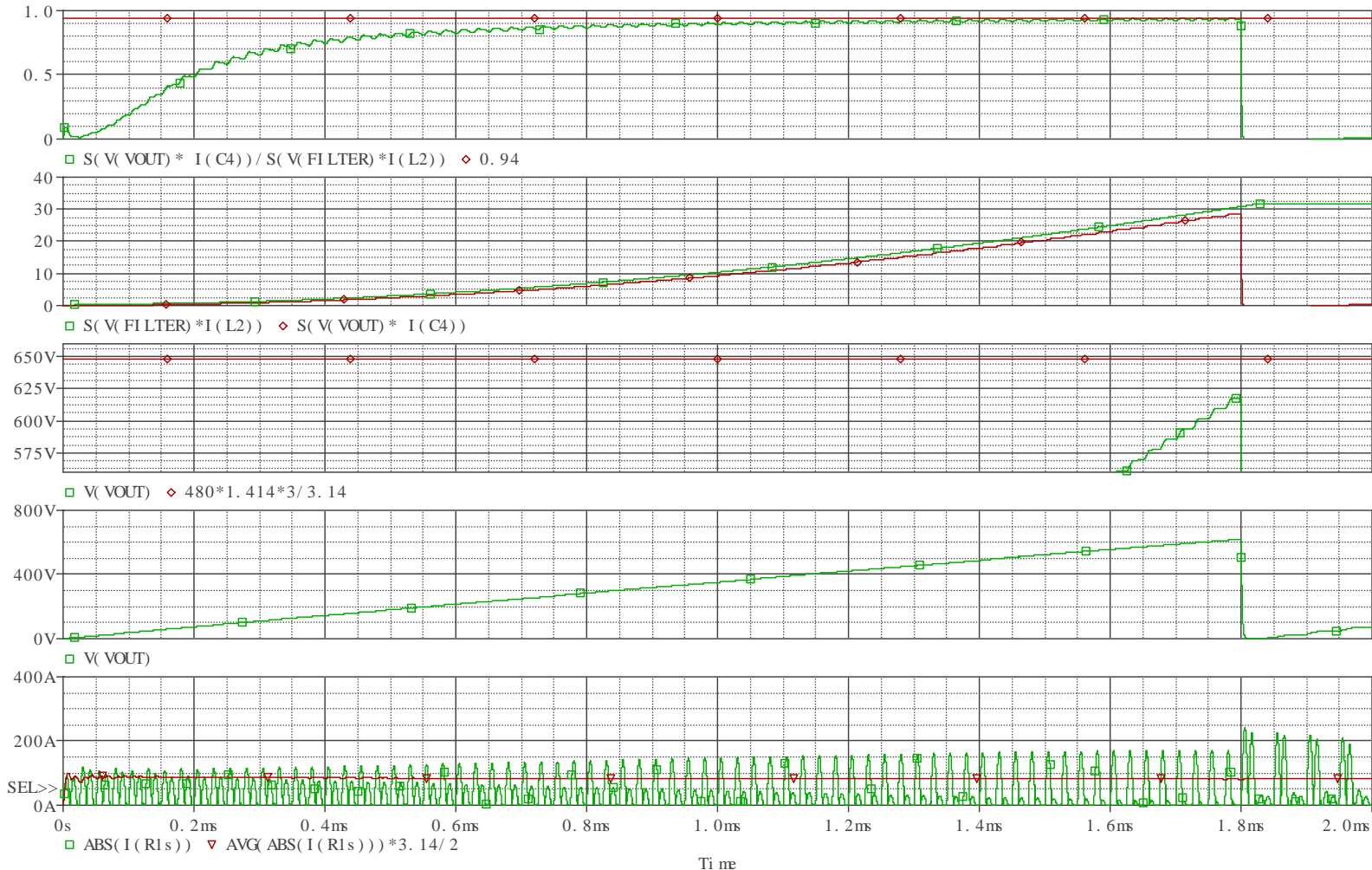
Internal Volume; 11 l



Circuit Diagram of PSPICE Simulation



Circuit Analysis by PSPICE Simulation



Time

Power Loss & Efficiency

Power Loss

IGBT; $2V_{ce} I_{av} + 2V_f I_f + 0.5 Q_{rr} V_{rm} f_{sw}$

Snubber; $0.5 C_s V_{dc}^2 f_{sw} \times 3$

DC Bank; $2V_f I_{dc} + I_{rms}^2 ESR$

Resonant Capacitor; $2 \pi f C V_{rms}^2 \tan \delta = I_{rms}^2 ESR$

Primary Winding; $R_{dc} I_{rms}^2$

Secondary Winding; $R_{dc} I_{rms}^2$

Ferrite Core; $k f[\text{kHz}]^{1.3} B[\text{mT}]^{2.5} \text{Volume}[\text{m}^3] / 3.5$

Rectifier; $2V_f I_f + 0.5 Q_{rr} V_{rm} f_{sw}$

Output Power **15 kW**
Power Loss **1.2 kW**
Efficiency **92.7 %**

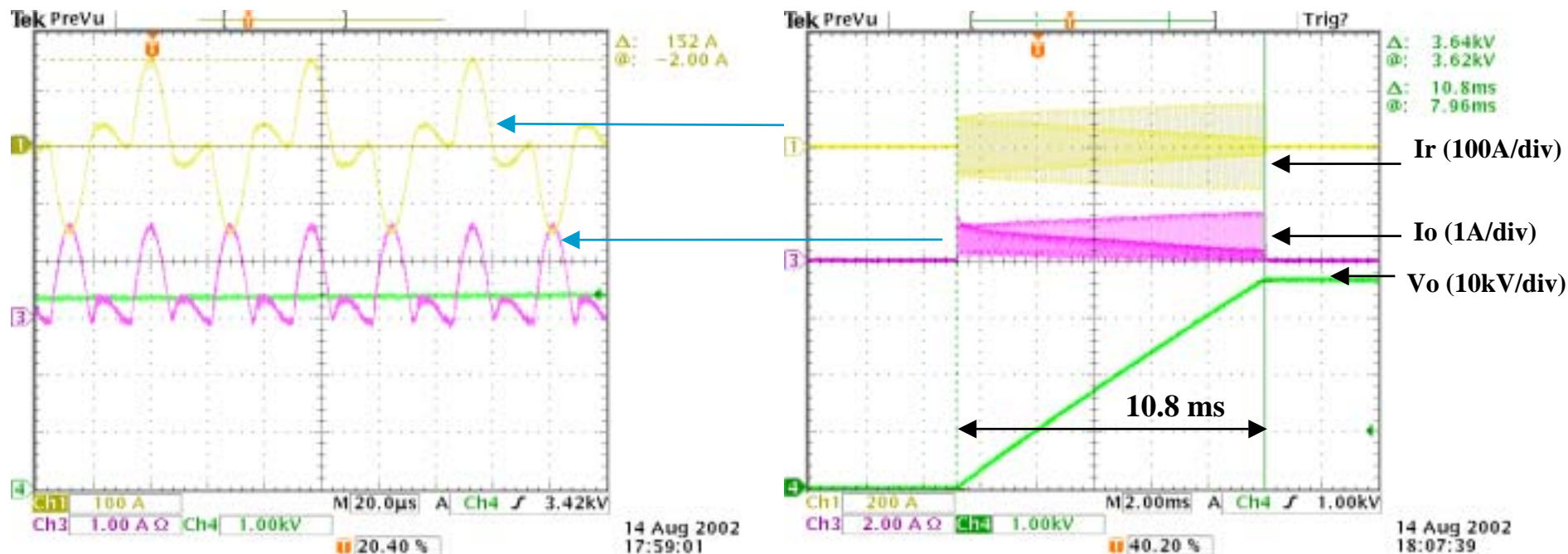
IGBT	242 W
Resonant Capacitor	44 W
Snubber	217 W
DC Bank	70 W
Others	120 W

Sub Total (Air)	693 W
Core	122 W
HV Rectifier	124 W
Trans. Winding	247 W

Sub Total (Oil Tank)	493 W

Measurement Waveform[1]

(Load Capacitance = 216 nF)



Expanded View

Horizontal : 20 us/div

Vertical : 10 kV/div

Horizontal : 2 ms/div, Vertical : 10 kV/div

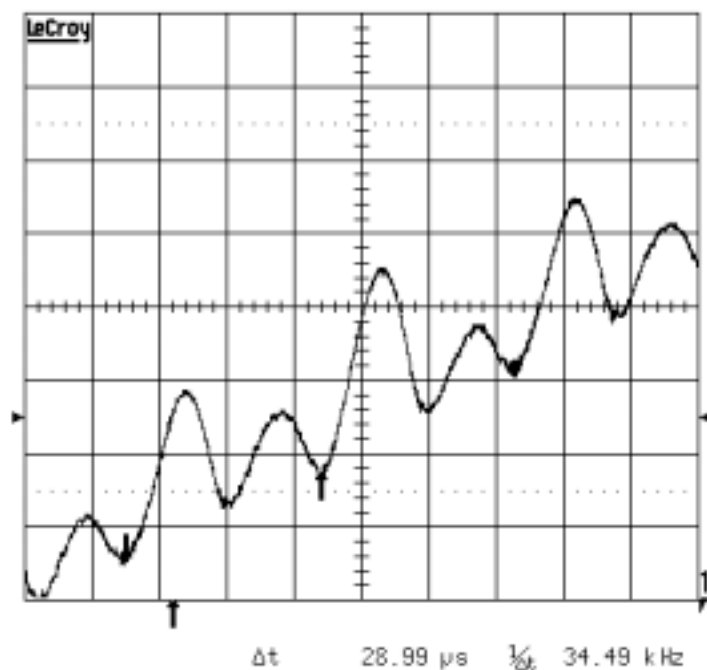
Output Current = 0.73 A

Charging Power = 13.2 kJ/sec

Peak Charging Power = 18.2 kJ/sec

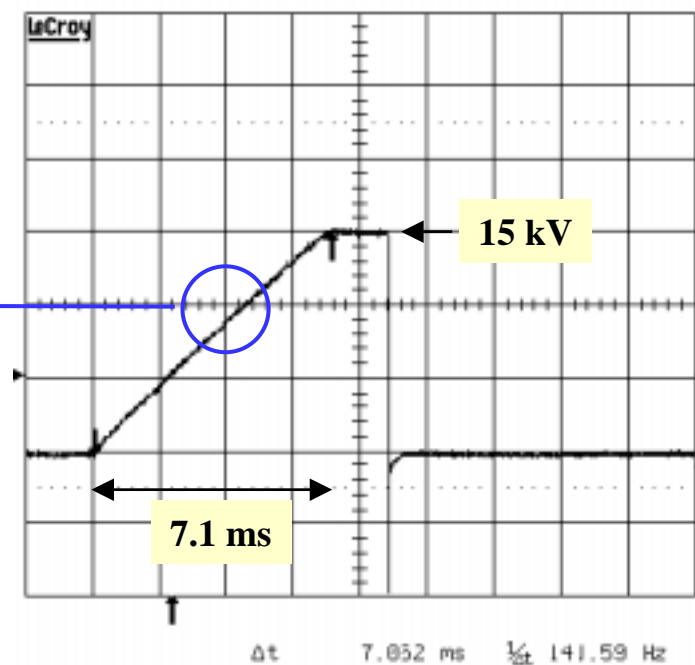
Measurement Waveform[2]

(Load Capacitance = 352 nF)



Expanded View

Horizontal : 10 $\mu\text{s}/\text{div}$, Vertical : 50 V/div
Resonant Frequency = 35 kHz



Horizontal : 2 ms/div, Vertical : 5 kV/div
Output Current = 0.74 A
Charging Power = 5.7 kJ/sec
Peak Charging Power = 18.6 kJ/sec

Summary

1. Air cooling for simplicity.
2. Resonant parameters; $f_r = 35$ kHz, $L_r = 29$ μ H, $Z_r = 6.5$ Ω .
3. Peak charging power is 18 kJ/sec with 0.72 A.
4. Average power is 15 kW with 83% duty factor.
5. Total power loss is estimated to be 1.2 kW.
6. System efficiency is about 93%.
7. Cooling capacity of oil tank is 500 W by forced convection.
8. The cooling capability of HV oil tank is limiting factor.