



# Prototype Measurements of Coupler Cavities for L-band Traveling-wave Accelerating Structure\*

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POSTECH  
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\*Work Supported by KAPRA and PAL

# Introduction



- L-band traveling-wave electron accelerator
- Irradiation Application
- 1.3 GHz, 10 MeV and 30 kW
- Design by SUPERFISH and PARMELA code
- Prototype measurements of coupler cavities
- Kyhl's method

# Accelerator Parameters

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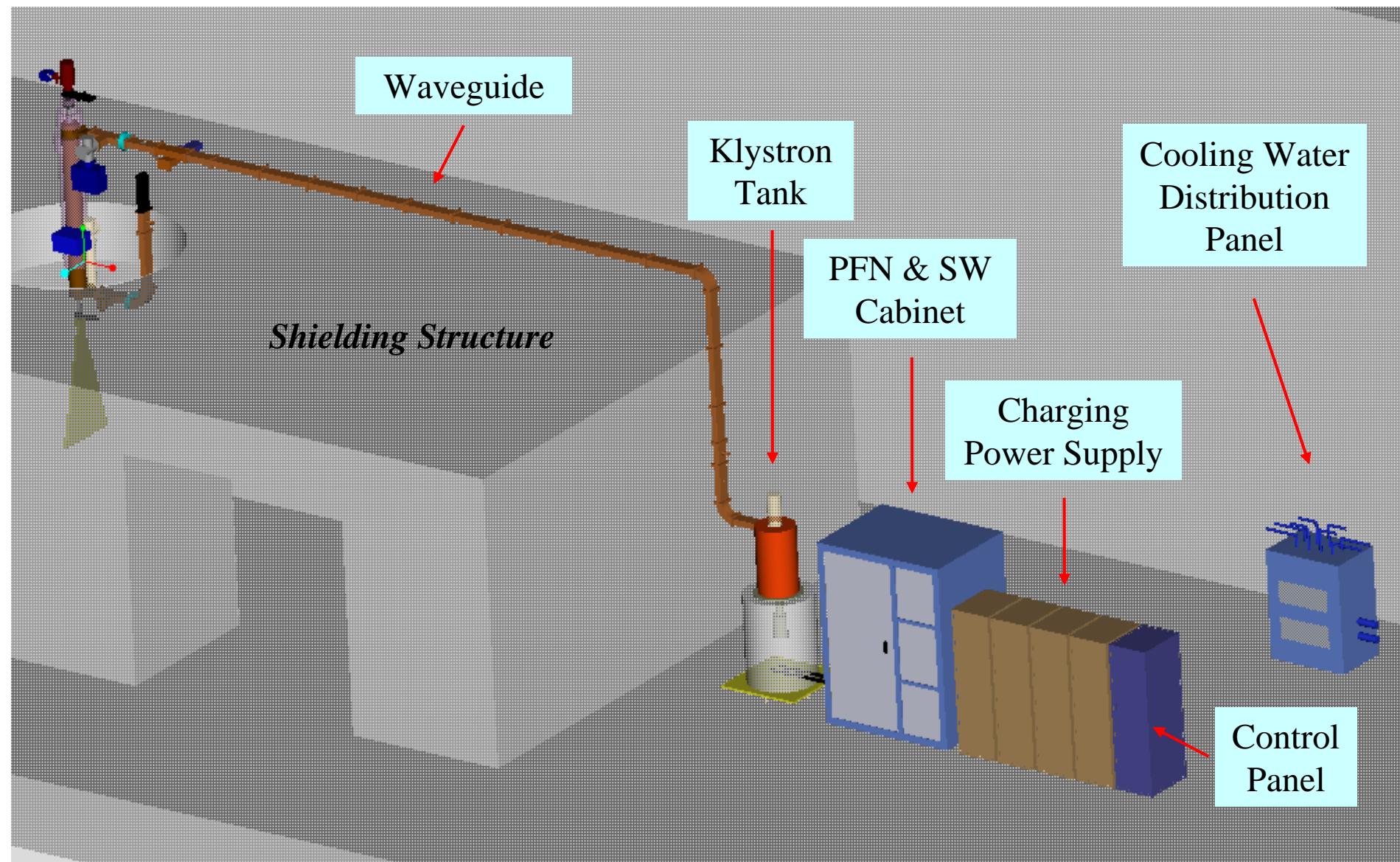
<b>Beam</b>		<b>E-gun</b>	
Beam Species	Electron	High Voltage	80 kV
Beam Energy	10.3 MeV	Pulsed Beam Current	1.6 A
Pulsed Beam Current	1.45 A	Beam Duty Factor	$2.1 \times 10^{-3}$
Beam Transmission Rate	91%	<b>RF</b>	
Beam Duty Factor	$2.1 \times 10^{-3}$	Operating Frequency	1300 MHz
Averaged Beam Power	31.4 kW	Pulsed RF Power	25 MW
No Loaded Beam Energy	17 MeV	RF Duty Factor	$2.38 \times 10^{-3}$
Beam Loading Factor	-4.62 MeV/A	Averaged RF Power	60 kW

# Accelerator Parameters

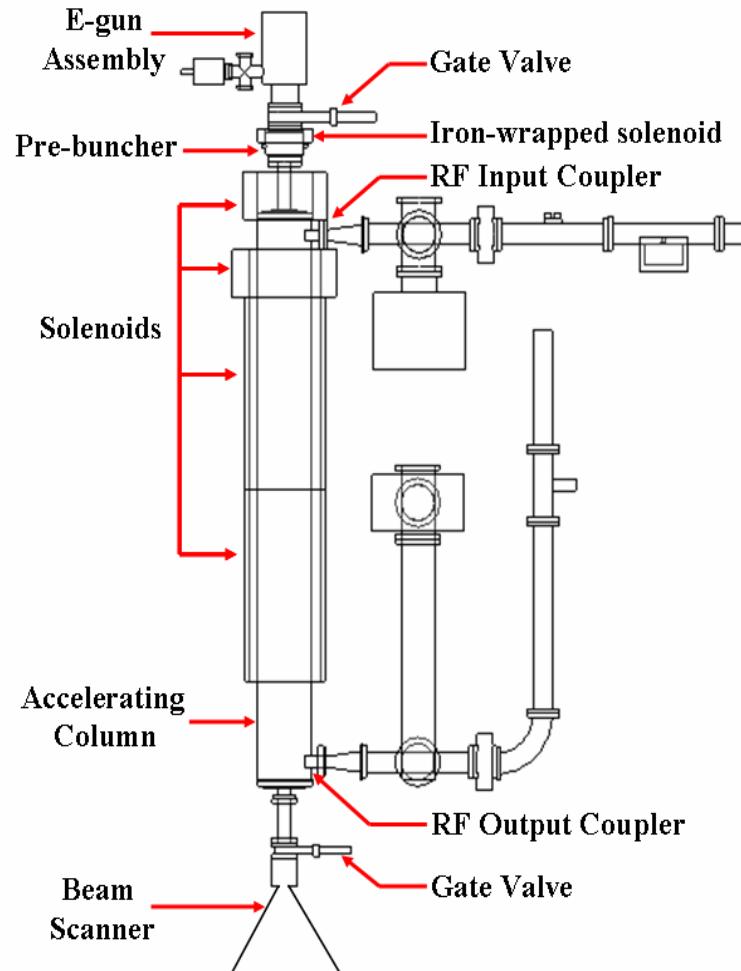
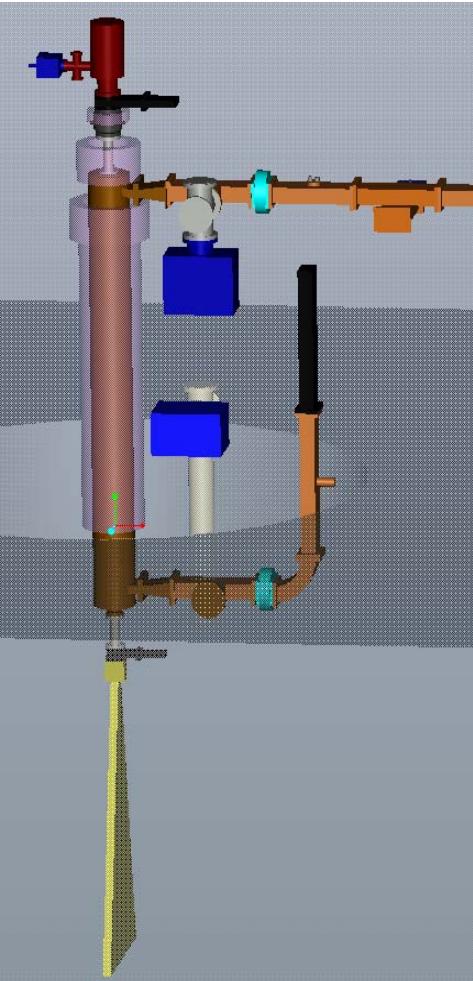
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Accelerator Structure	
Number of Bunching Cells	5
Number of Accelerating Cells	26
Total Length	2.4 m
Operating Mode	$2\pi/3$
Operating Temperature	$40^\circ\text{C} \pm 1^\circ\text{C}$
Averaged Accelerating Gradients	4.2 MV/m
Shunt Impedance*	43 MΩ/m
Quality Factor*	20000

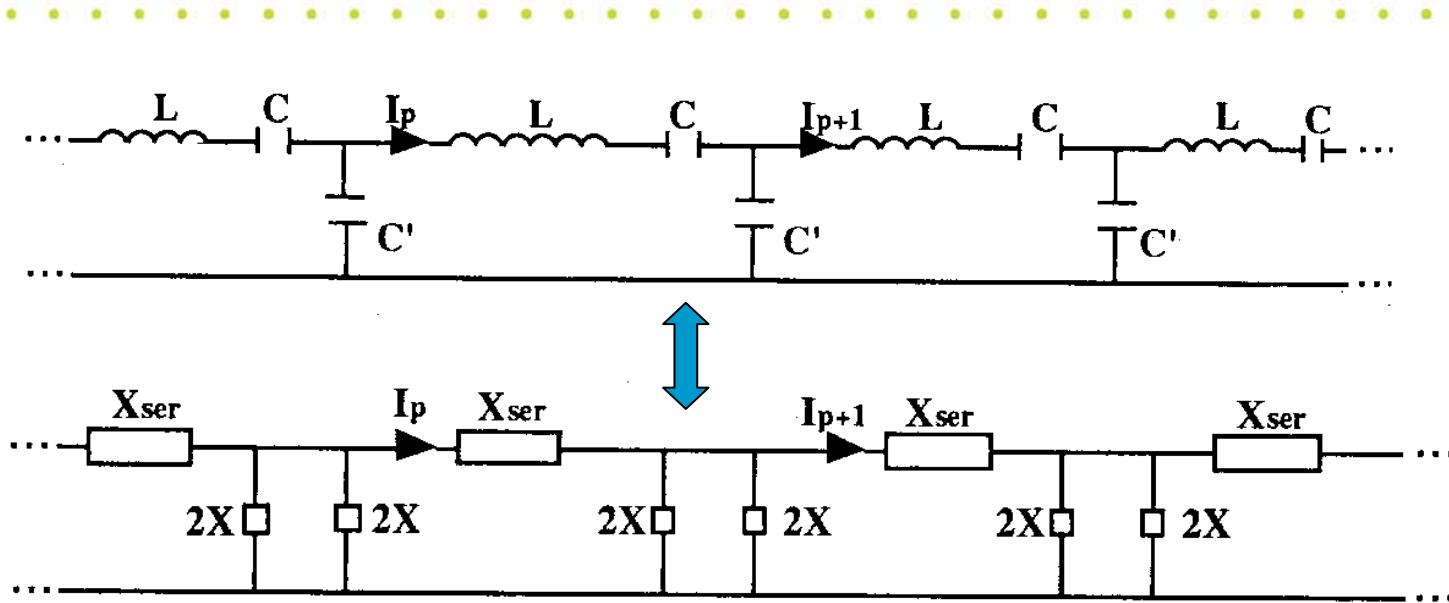
# Layout of Accelerator System



# Layout of Beamline



# Input Impedance for Traveling-wave Accelerating Structure



For no reflected wave and the phase advance of  $\theta$  per cell

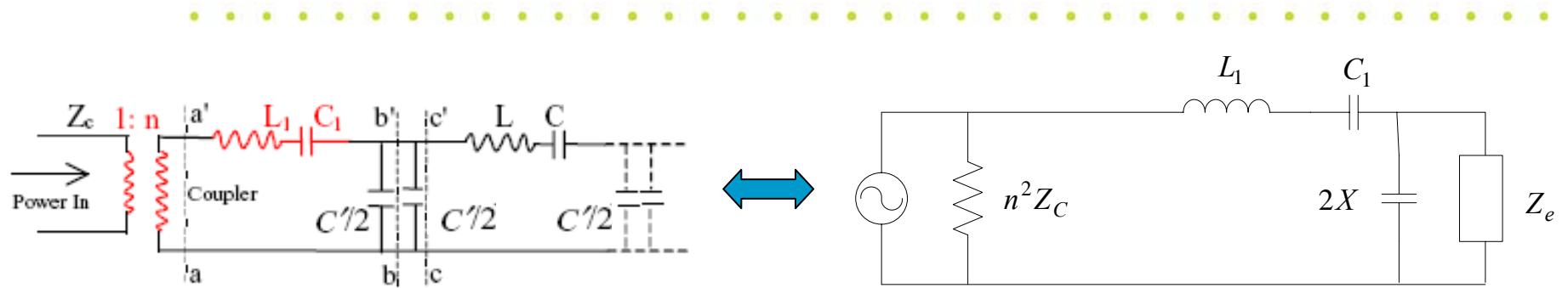
$$Z_e^2 = \frac{X \cdot X_{ser}}{1 + \frac{X_{ser}}{4X}}, \quad \cos \theta = 1 + \frac{X_{ser}(\omega_\theta)}{2X(\omega_\theta)} \quad \Rightarrow \quad Z_e^2(\omega_\theta) = -4X^2(\omega_\theta) \tan^2 \frac{\theta}{2}$$

$$Z_e(\omega_\theta) = 2|X(\omega_\theta)| \tan \frac{\theta}{2}$$

$Z_e$  : Input impedance of periodic array of traveling-wave accelerating cells

$$X_{ser} = j\omega L + \frac{1}{j\omega C}, \quad X = \frac{1}{j\omega C'}$$

# Matching Condition for Traveling-wave Accelerating Structure



$$Z_L = n^2 Z_C$$

$$Z_R(\omega_\theta) = j\omega_\theta L_1 + \frac{1}{j\omega_\theta C_1} + \frac{2X \cdot 2|X| \tan(\theta/2)}{2X + 2|X| \tan(\theta/2)} = |X| \sin \theta + j|X| \left( \frac{4\delta}{k} + \cos \theta \right)$$

where  $\delta = \frac{\omega_C}{\omega_{\pi/2}} - 1$ ,  $\omega_C = \sqrt{\frac{1}{L_1 \nu}}$ ,  $\frac{1}{\nu} = \frac{1}{C_1} + \frac{1}{C'}$

Matching condition:  $Z_L = Z_R$

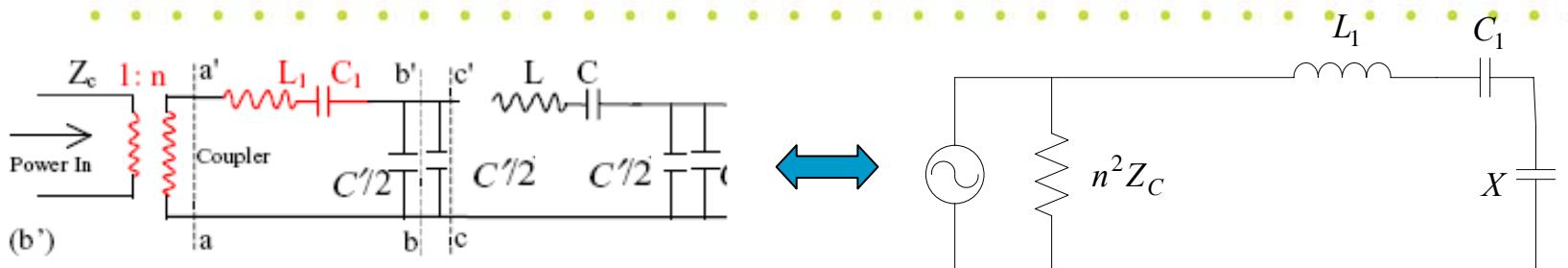
$$\beta \equiv \frac{n^2 Z_C}{|X(\omega_\theta)| \sin \theta} = 1$$

$$\omega_C = \omega_{\pi/2} \left( 1 - \frac{k}{4} \cos \theta \right) \cong \frac{\omega_{\pi/2} + \omega_\theta}{2}$$

Dispersion relation

$$\omega_\theta = \frac{\omega_{\pi/2}}{\sqrt{1 + k \cos \theta}}$$

# Analysis of Kyhl's Method



$$\tan \frac{\varphi}{2} \cong \frac{n^2 Z_C}{\omega L_1 - \frac{1}{\omega \nu}} = \frac{n^2 \omega Z_C}{L_1 (\omega^2 - \omega_C^2)} \quad , \text{ when } |\Gamma| \rightarrow 1$$

$$\beta = \frac{1}{\frac{k}{2} \omega_{\pi/2} \sin \theta} \cdot \frac{\tan \frac{\varphi_1}{2} \tan \frac{\varphi_2}{2} (\omega_1^2 - \omega_2^2)}{\omega_1 \tan \frac{\varphi_2}{2} - \omega_2 \tan \frac{\varphi_1}{2}}$$

$\omega_1, \omega_2$  are arbitrary frequencies and  
 $\varphi_1, \varphi_2$  are corresponding reflection angles.

For matched condition, the resonant frequency of this circuit should be as following.

$$\omega_C \cong \frac{\omega_{\pi/2} + \omega_\theta}{2}$$

If we choose frequencies as  $\omega_1 = \omega_{\pi/2}$ ,  $\omega_2 = \omega_{2\pi/3}$  then  $\varphi_1 = -\varphi_2$  and

$$\beta \cong \frac{\tan(\varphi_1/2)}{\sqrt{3}} = 1.$$

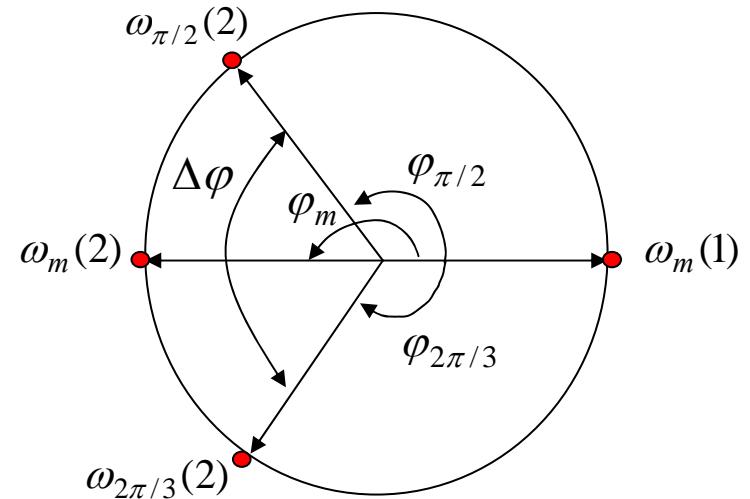
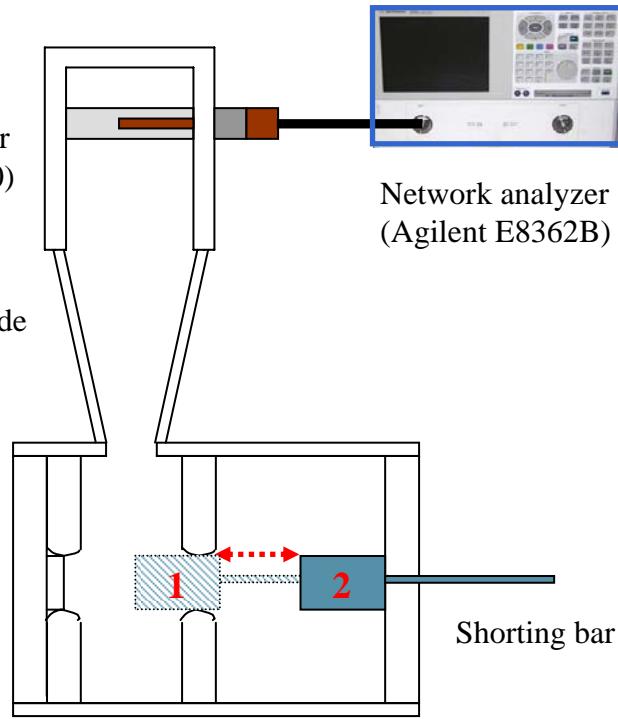


Equivalent to Kyhl's method

# Impedance Matching for coupler cavities

Coaxial to waveguide adapter (N-type to WR650)

Tapered waveguide (1/3 reducing)



$\omega_m(1)$  : mean frequency of  $\omega_{\pi/2}$  and  $\omega_{2\pi/3}$  at position 1

$\omega_{\pi/2}(2)$  :  $\pi/2$ -mode frequency at position 2

$\omega_{2\pi/3}(2)$  :  $2\pi/3$ -mode frequency at position 2

$\omega_m(2)$  : mean frequency of  $\omega_{\pi/2}$  and  $\omega_{2\pi/3}$  at position 2

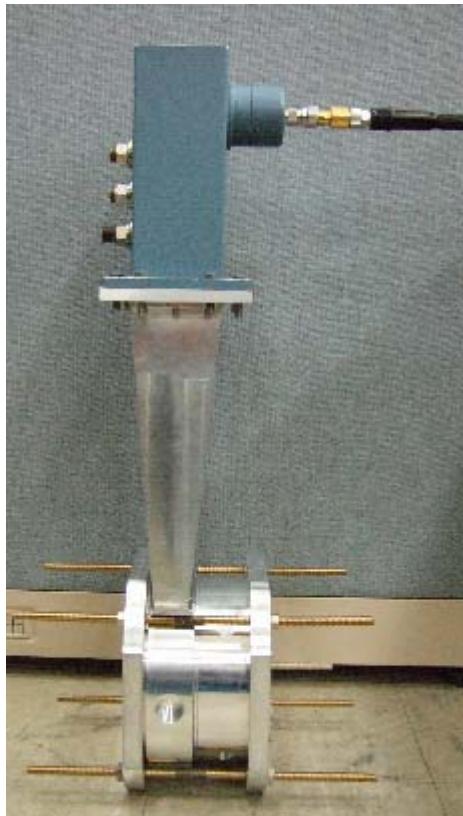
For critical coupling to traveling-wave accelerating column

$$\varphi_m = 180^\circ \quad \varphi_{\pi/2} = \varphi_{2\pi/3} = 120^\circ$$

Under-coupled:  $\varphi_{\pi/2} = \varphi_{2\pi/3} < 120^\circ$

Over-coupled:  $\varphi_{\pi/2} = \varphi_{2\pi/3} > 120^\circ$

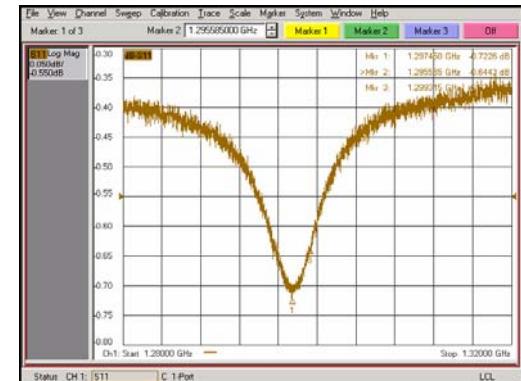
# Prototype Test of Coupler Cavities



Setup for Prototype Test



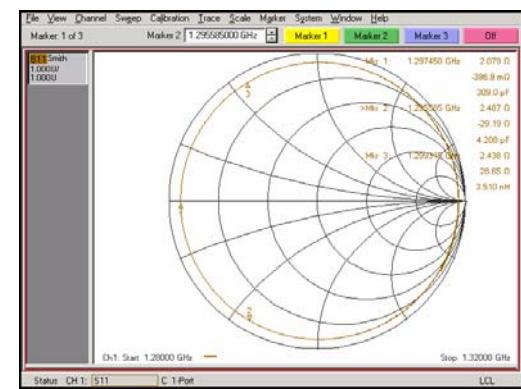
Network Analyzer



S11 Parameter

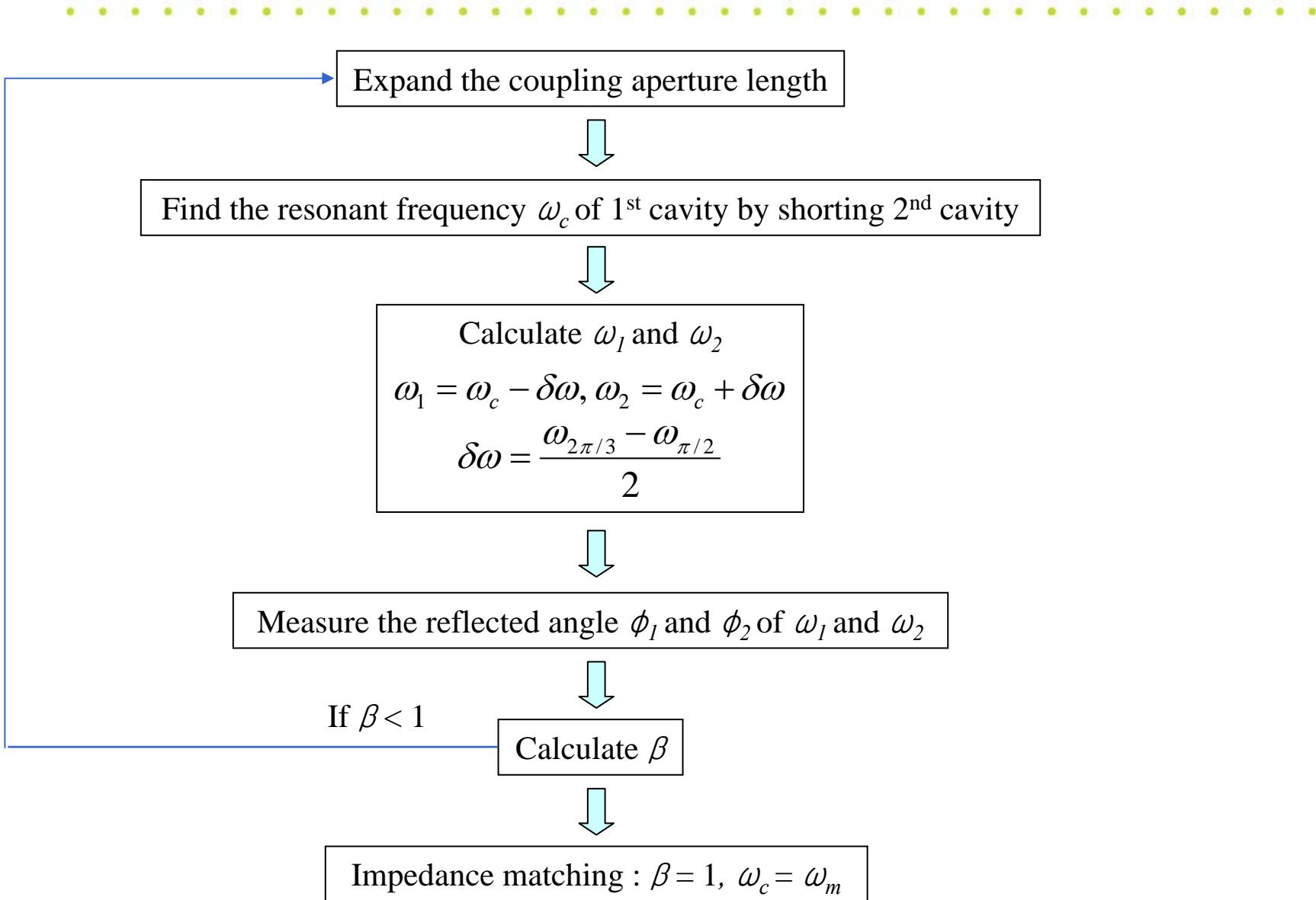


Phase

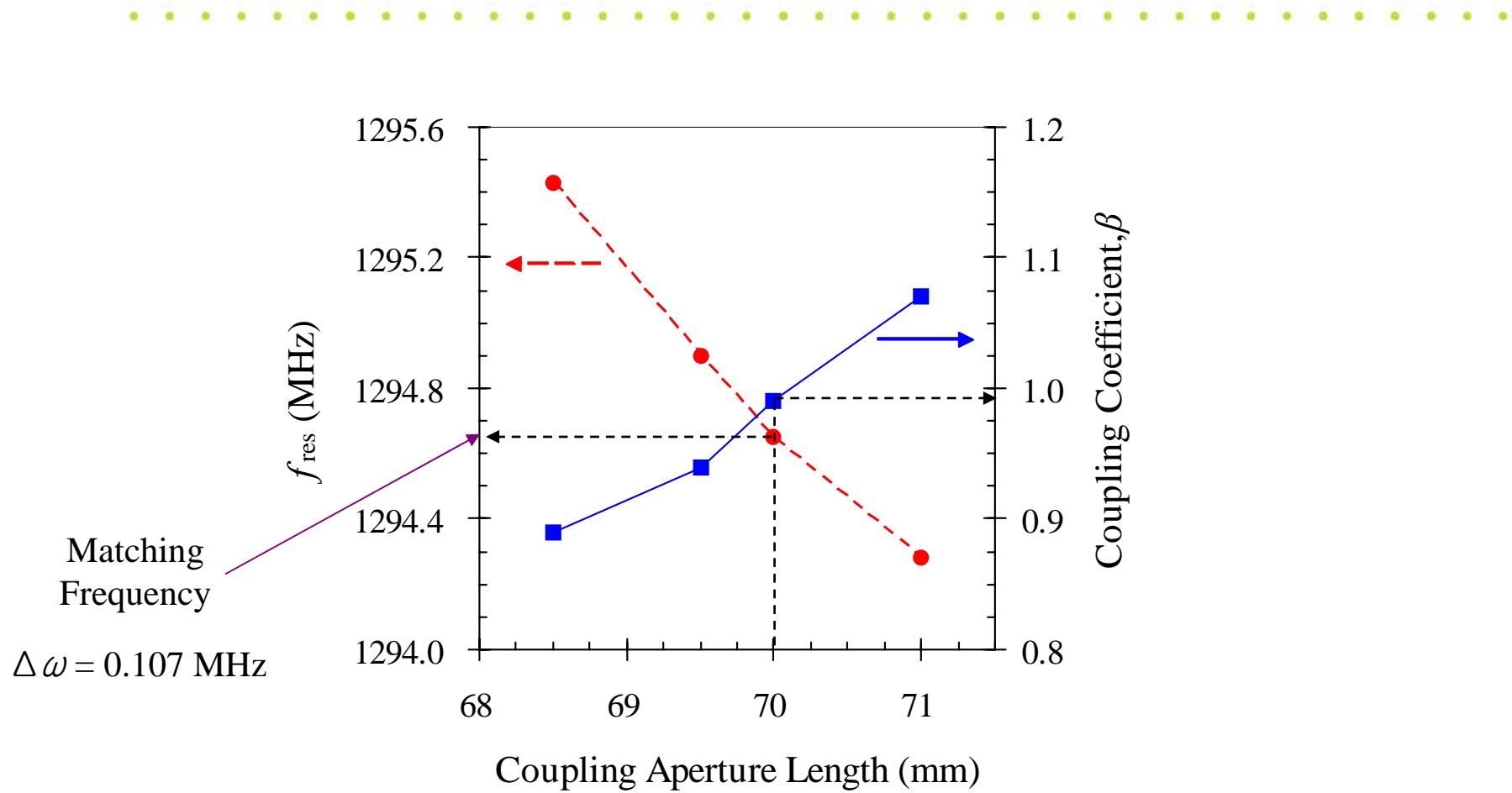


Smith Chart

# Measurement Procedure

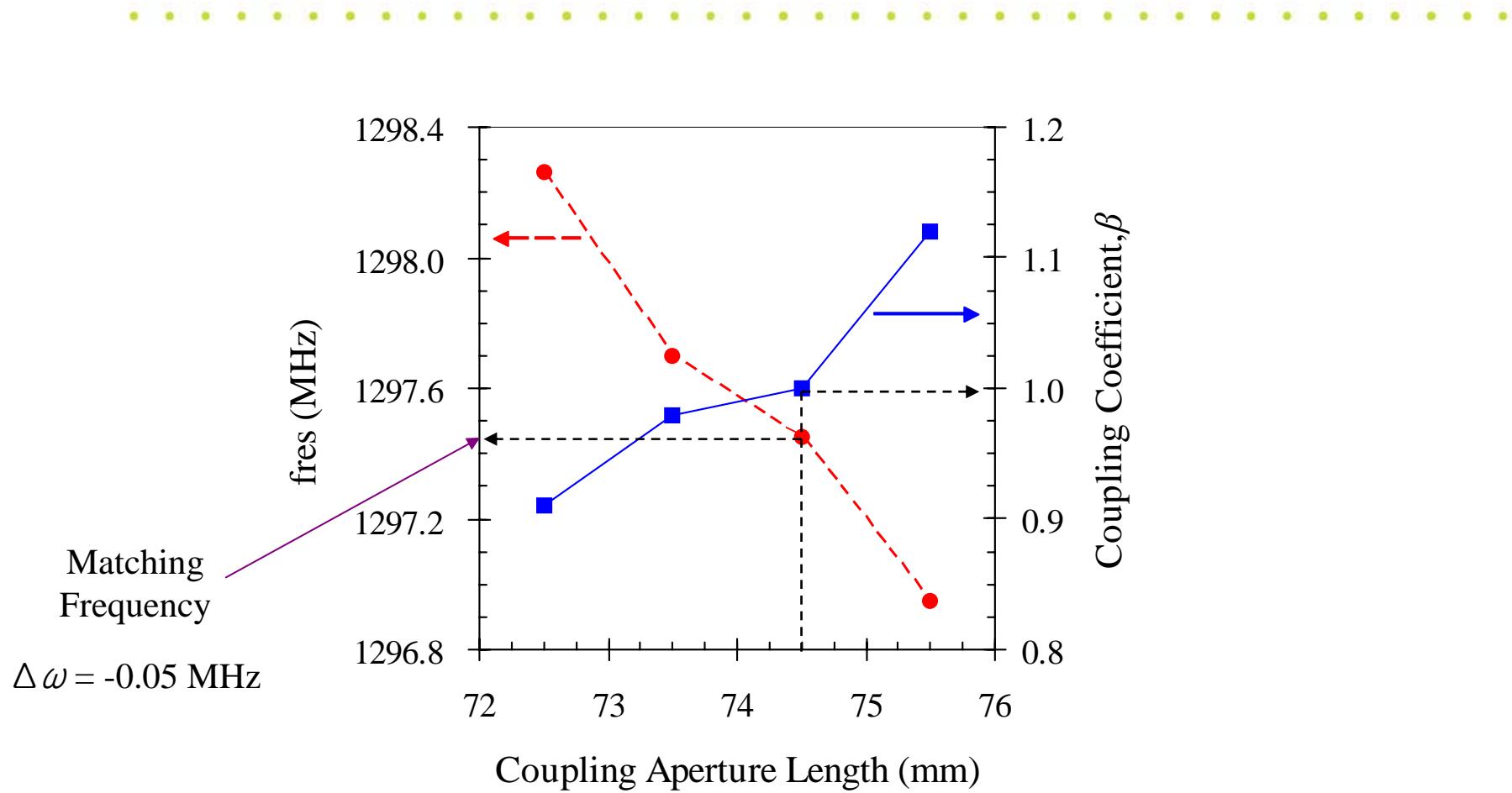


# Experimental Results of Input Coupler



Cavity radius and coupling aperture width are fixed.

# Experimental Results for Output Coupler



Cavity radius and coupling aperture width are fixed.

# Summary



- Intense L-band traveling-wave linac of 10 MeV and 30 kW is designed for the sterilizing industrial application.
- Impedance matching for input and output coupler cavities are tested by the Khyl's method.
- With cold tests of model cavities, detailed dimensions are confirmed for the fabrication drawings.